

Progress in Reducing Vibration Levels on NPSCuL

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NPSCuL Overview

- NPSCuL is an ESPAcompatible payload with a capacity of 24 1U CubeSats using P-PODs and 6U dispensers
- 2 successful launches, OUTSat and GEMSat, on the Atlas V Aft Bulkhead Carrier (ABC) in 2012 and 2013
- 2 upcoming launches, ULTRASat and GRACE, in May and August 2015



Need for Reducing Vibration Levels

- "Test-To-Insane Levels" (TTIL) methodology applied to CubeSats on NPSCuL during random vibe
 - \circ ~15 G_{RMS} at MPE for the P-POD is considered harsh
 - Rigidly mounted, cantilevered, thin-plate structure causes amplification at P-POD interface
- Discourages more sensitive and complex payloads from gaining access to space via ABC
 - Current environment is considered "coach-class"



X-Axis G_{RMS} (Worst-Case)

Level	Base (Input)	P-POD Interface*	
Acceptance (MPE +0dB)	7.6	15.1	
Protoqual (MPE +3dB)	10.7	21.4	
Qual (MPE +6dB)	15.2	30.3	
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*Envelope of OUTSat acceptance test data (Flight P-PODs and CubeSats)

Progression of Vibration Reduction Methods for NPSCuL

- Implemented force-limited vibration testing (FLVT) to minimize over-test caused by test set-up
 - Effective in reducing the resonance at the fundamental frequency
- Redesigned NPSCuL to increase stiffness
 - Moves fundamental frequency from ~50 Hz to ~75 Hz
 - $\circ~$ Increased stiffness results in reduced benefit from FLVT in overall G_{RMS} for the ABC input
- Obtain lower input from LV provider
 - No flight data for full test frequency range available to create test envelope

FLVT on NPSCuL

- Semi-empirical method is used to calculate force limit per NASA-HDBK-7004B
 - Has been repeatedly shown to be the least conservative method while still meeting test requirements
- Results in a notch in the acceleration input at the fundamental frequency
- Force roll-off is assumed after fundamental frequency to 500 Hz
- Does not provide relief past the forcelimited range
 - Test data shows there is a significant amount of energy above 500 Hz at the P-POD interface
 - Not a mechanism, and is not intended to be, for changing the resonant properties of the system





Redesigned NPSCuL - Isogrid

- Isogrid techniques were utilized to reduce amplification by increasing stiffness without increasing overall mass
 - Moves fundamental frequency from ~50 Hz to ~75 Hz
- NPSCuL adapter ring and base plate were unified into a single part to reduce amplification from "rocking" modes
- Increased stiffness results in reduced benefit from FLVT in overall G_{RMS} for the ABC input
- No significant change in G_{RMS} between isogrid and baseline NPSCuL when using FLVT set-up





***Reference:** Kaushish, V., "Force limited vibration testing and subsequent redesign of the Naval Postgraduate School CubeSat launcher," Monterey, CA: Naval Postgraduate School, 2014.

Next Step – Isolators on NPSCuL

- Implement isolators with FLVT to reduce P-POD environment on NPSCuL
- Eight (8) COTS isolators incorporated between adapter ring and baseplate
- Attaches to the LV interface using eight (8) of the 24 fastener locations on the 15" ESPA standard



Isolator Installation Configurations

- Conical broad-temperature-range (BTR) silicone isolators (LORD AM-009-14) constrained using two (2) methods
 - Method 1: Fastener that goes through supported unit is threaded into supporting member
 - Elastomer is constrained in compression, tension, and shear
 - Effectively lowers the CG of NPSCuL by 0.9" with little reduction in joint stiffness
 - Method 2: Typical installation for true isolation behavior
 - Elastomer is allowed to deflect as intended by vendor
 - Generally recommended for use in compression only
 - Significant change to joint stiffness and lowers the CG
 - Use in tension is assessed on a case-by-case basis



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Isolator Test Set-Up

- All NPSCuL configurations, integrated with 8 P-POD Mass Models (P2M2s) and a SAD EDU, were subjected to the following tests in each axis
 - Fixed-base 0.5 G sine sweep, 20-2000 Hz
 - Un-notched and force-limited ABC levels, 7.6 Grms random acceleration input (MPE)
 - FLVT is still necessary to reduce conservatism during test
- Configurations are referred to as follows:
 - Config 1: Baseline (no isolators, original NPSCuL structure)
 - Config 2a: Baseline with constrained isolators (Method 1)
 - Config 2b: Baseline with isolators, typical installation(Method 2)



Dynamic Properties of Constrained Configuration

- Isolator system is not effective in lateral directions when constrained
 - First fundamental frequency in X, Y axes shifted lower by 15 Hz
 - Most likely attributed to a lower CG
- Isolators behave as expected in Z axis
 - Indicative of much lower response after the 1st fundamental mode



Apparent Mass (from Sine Sweep)

Dynamic Properties of Typical Installation Configuration

- Typical behavior for base-۲ mounted isolators on a box-like structure
 - Results in two (2) distinct 0 modes in each axis and no amplification of higher order modes
- Isolation system appears to ٠ produce a tuned-mass damper effect
 - Anti-resonance of isolated \cap system occurs at fundamental frequency of baseline NPSCuL
- Peak at 1560 Hz in Z-axis is • an FLVT plate mode
- Lower apparent mass • results in lower response in all axes

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Performance Summary

- Significant reduction in P-POD interface environment with isolated NPSCuL
 - \circ Lower CG only contributes ~30% of total G_{RMS} reduction
- Qualification G_{RMS} levels would be less than current acceptance G_{RMS}



Level	Base (Input)	P-POD Interface, Config 1	P-POD Interface, Config 2b
Acceptance (MPE +0dB)	7.6	15.9	6.2
Protoqual (MPE +3dB)	10.7	22.5	8.8
Qual (MPE +6dB)	15.2	31.8	12.4
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*Envelope of development test data (P2M2s)

X-Axis G_{RMS} (Worst-Case)

Combined Effects of FLVT and Isolation

- Isolation system alone is effective in reducing G_{RMS} , but conservatism is still further reduced with FLVT
- Force-limited vibration test setup is still beneficial and plays an integral part in reducing the P-POD response



Benefits for the CubeSat Community

- Provides a COTS isolation system for NPSCuL and CubeSats
 - Isolation system for larger satellites (greater than 500 lbs) exist, but are often mission-specific
 - Applicable to other ESPA-class spacecraft of similar size
- Cost of NPSCuL isolation system is ~\$2000 for 35-85% reduction in random vibration environment
 - Considerable cost reduction over existing industry customized spacecraft isolation for similar performance*
- Proposed isolation system is compatible with ESPA and PSC MLB interfaces and can be easily altered for use with any ESPA-class interface
 - Main design parameters include mass and mounting configuration on LV

*References:

Wilke, P., Johnson, C., Grosserode, P., Sciulli, D., *Whole-Spacecraft Vibration Isolation on Small Launch Vehicles*, Smart Structures and Materials 2000, Damping and Isolation, 2000.

Johnson, C., Wilke, P., Pendleton, S., SoftRide Vibration and Shock Isolation Systems that Protect Spacecraft from Launch Dynamic Environments, 38th Aerospace Mechanisms Symposium, 2006.

4/23/2015

Conclusion and Path Forward

- Effective and low-cost solution to provide a "first-class ride" to space for CubeSats and small spacecraft
 - Investigating other COTS isolators of comparable size that can be used in tension, compression, and shear without compromising isolator effectiveness
 - Typical isolator installation configuration in tension with current isolator may be investigated
- Qual test will be performed with final isolator selection



