



CubeSat Deformable Mirror Demonstration (CDMD)



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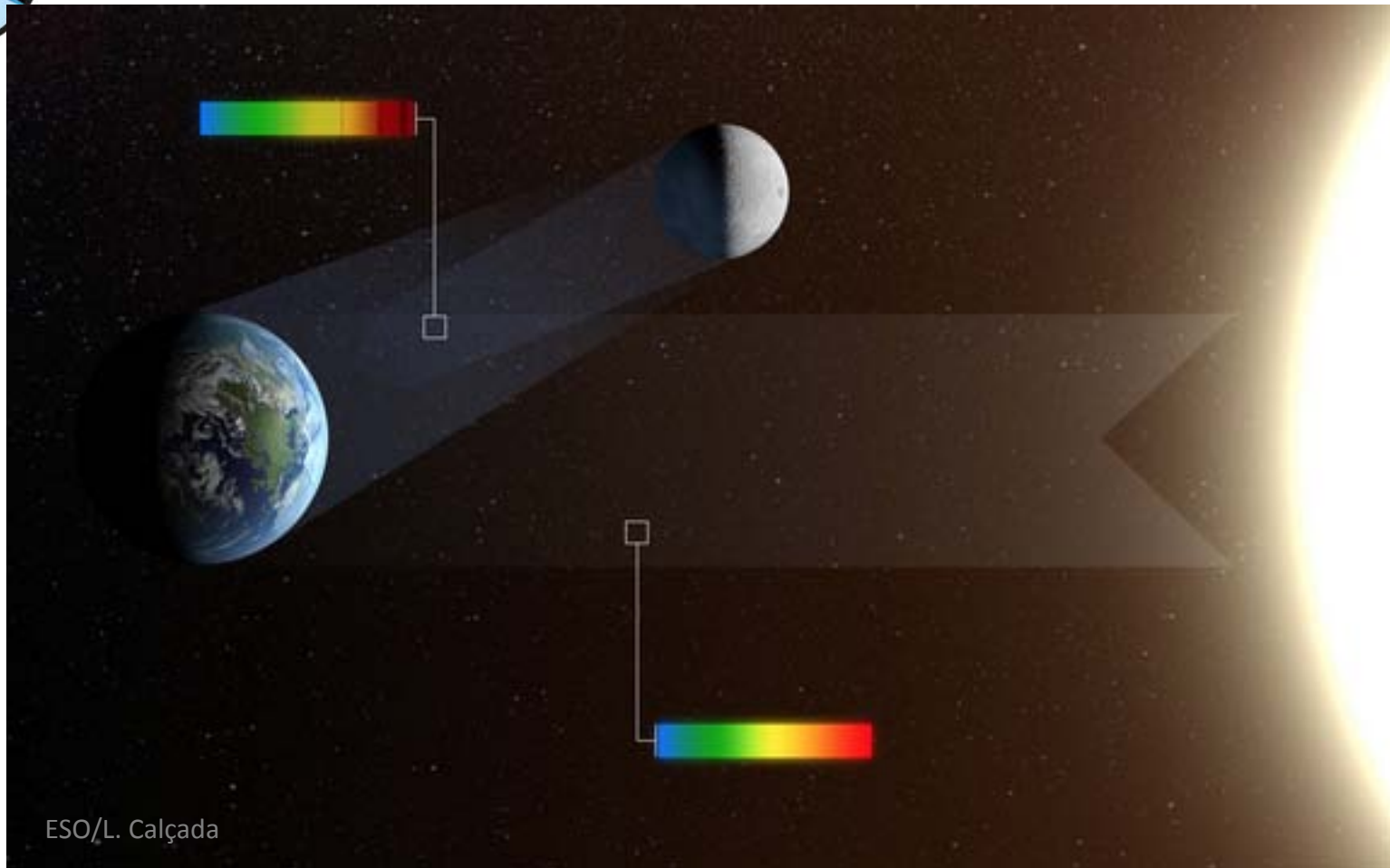
Is there *other* life out there?



earthobservatory.nasa.gov



Reflected starlight: spectra



- Look at absorption features in spectra: O₂, H₂O

But stars are really bright...





- Must block starlight to see planets around star



Coronagraph



- Use a coronagraph to block the star's light



Basic Coronagraph Optics

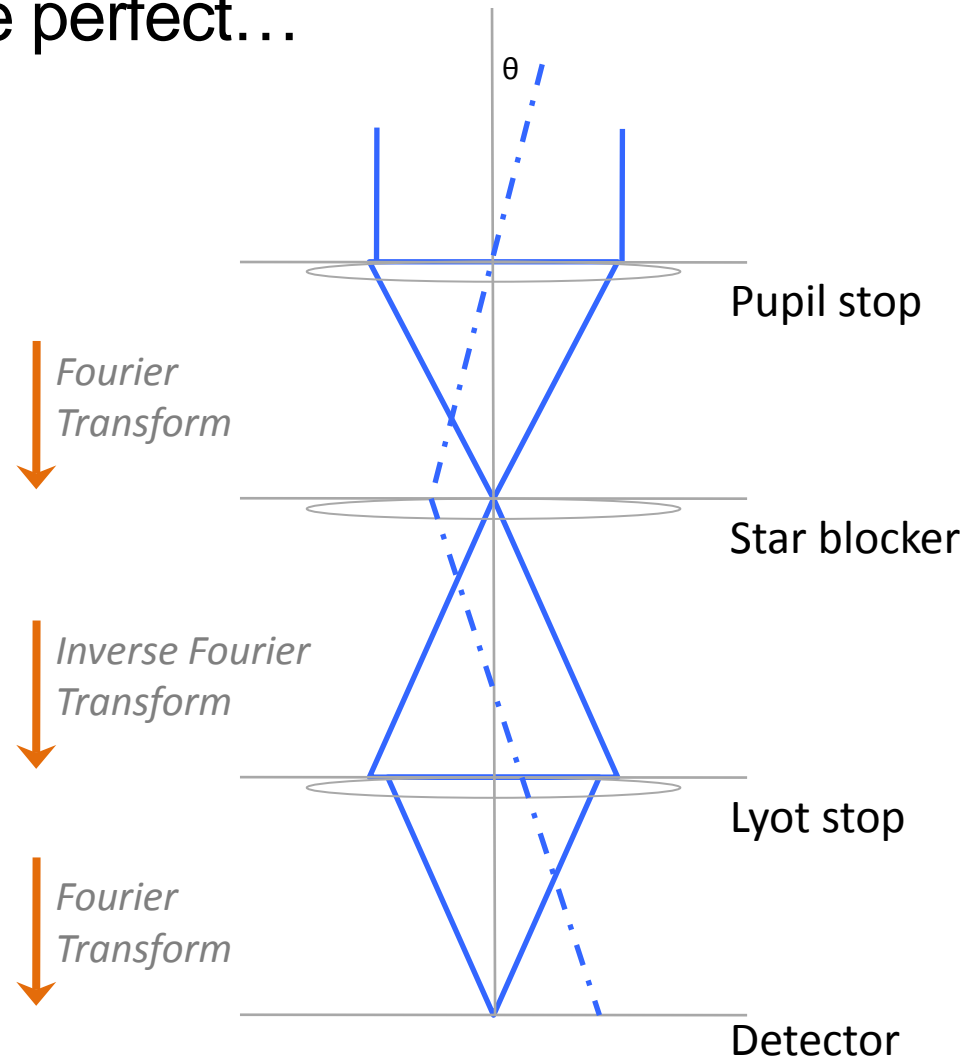
- If life were perfect...

1. Input Pupil

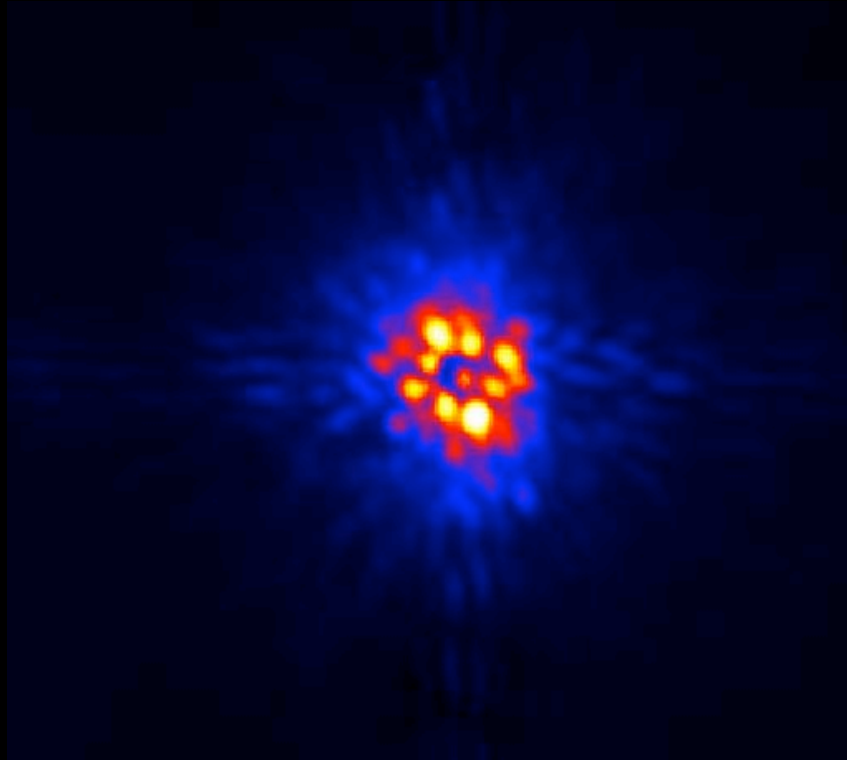
2. Image Plane

3. Reimaged Pupil

4. Reimaged...
Image Plane



But life is not perfect: speckles



The star 55 Cancri observed with the Lyot Project coronagraph at AEOs in Maui. The symmetric "speckles" arising from atmospheric effects and imperfections in the telescope optics are clear.
<http://www.lyot.org/results>



Corrupting an innocent wavefront

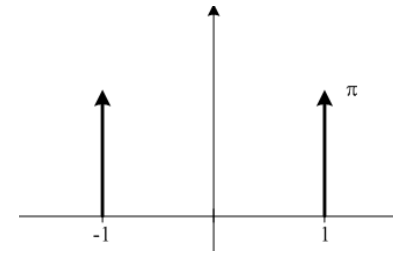
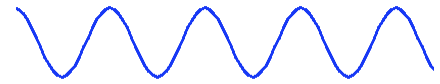
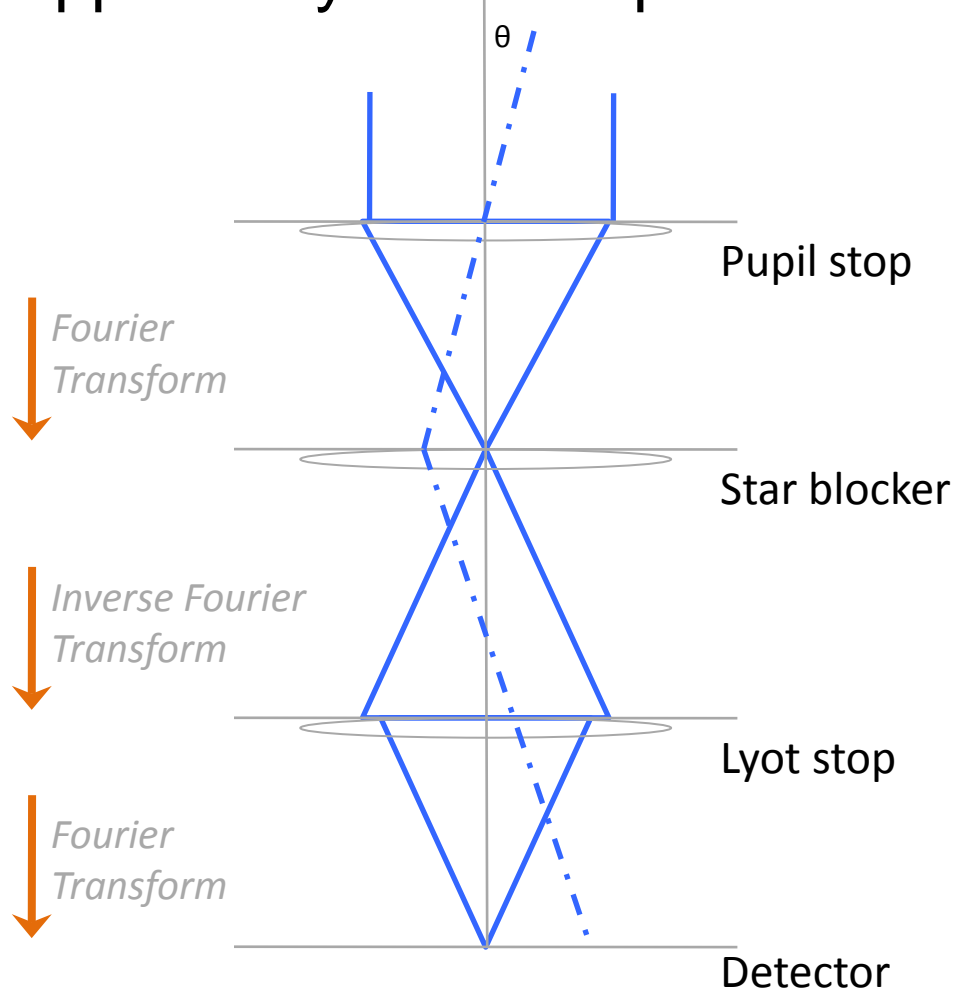
- Cosine ripple \rightarrow symmetric speckles

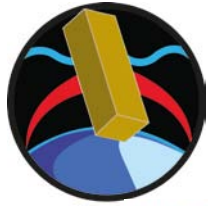
1. Input Pupil

2. Image Plane

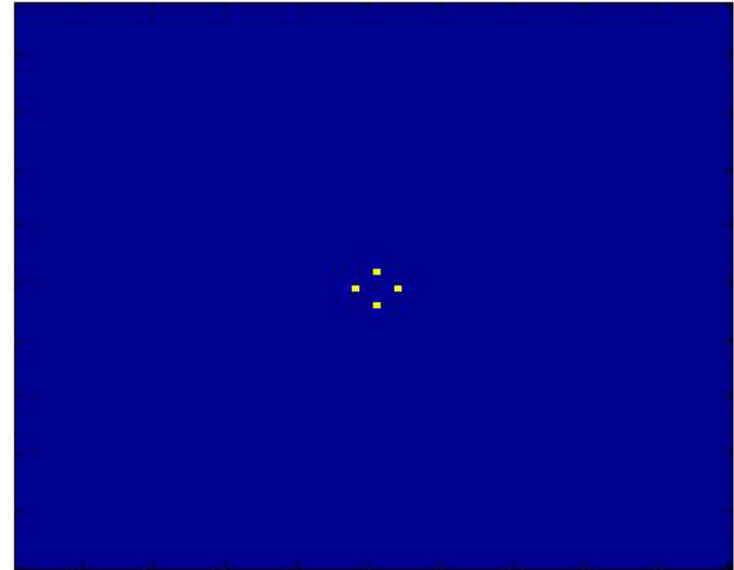
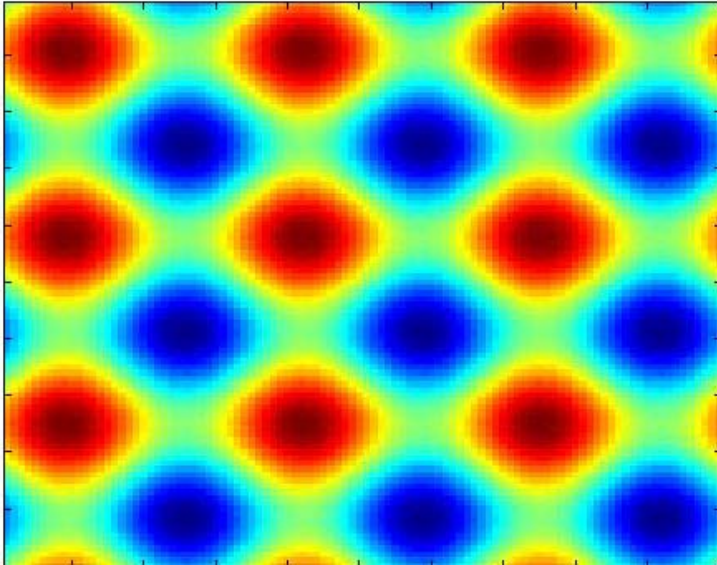
3. Reimaged Pupil

4. Reimaged...
Image Plane





2D Speckles

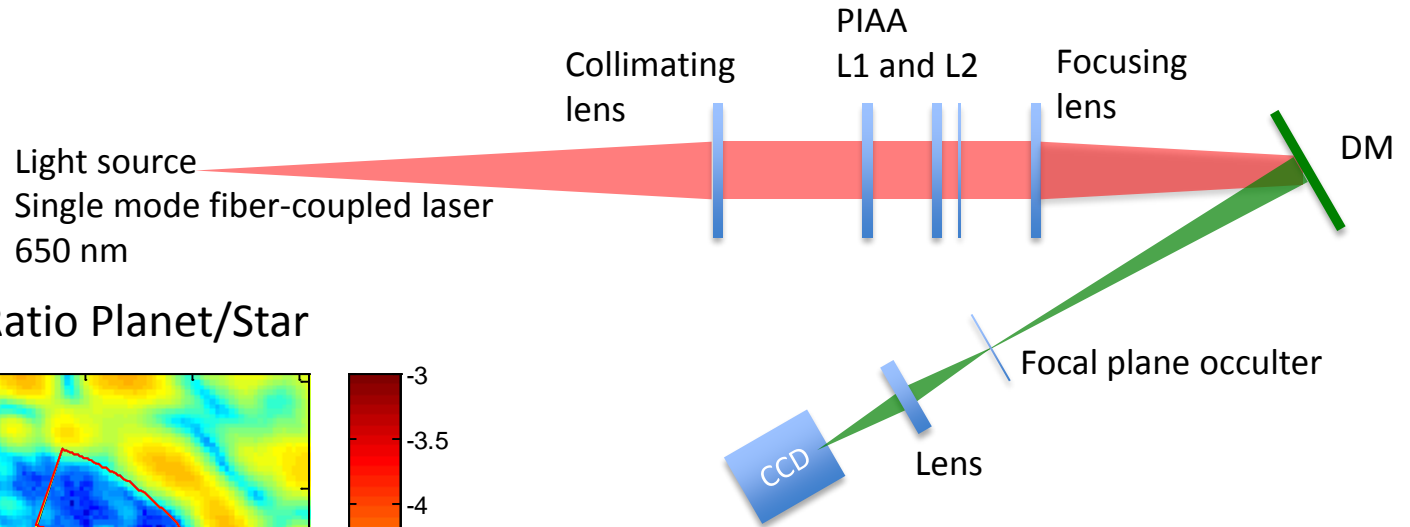


- 2D FFT of X, Y ripple pattern (e.g. surface error, stray light)
- Lower spatial frequencies at center, higher outside
 - Outside is where planets will be, need dark hole → Deformable Mirror
- N actuators per side of a DM, null $N/2$ waves, $\theta(\text{dark hole}) = \pm N\lambda / 2D$

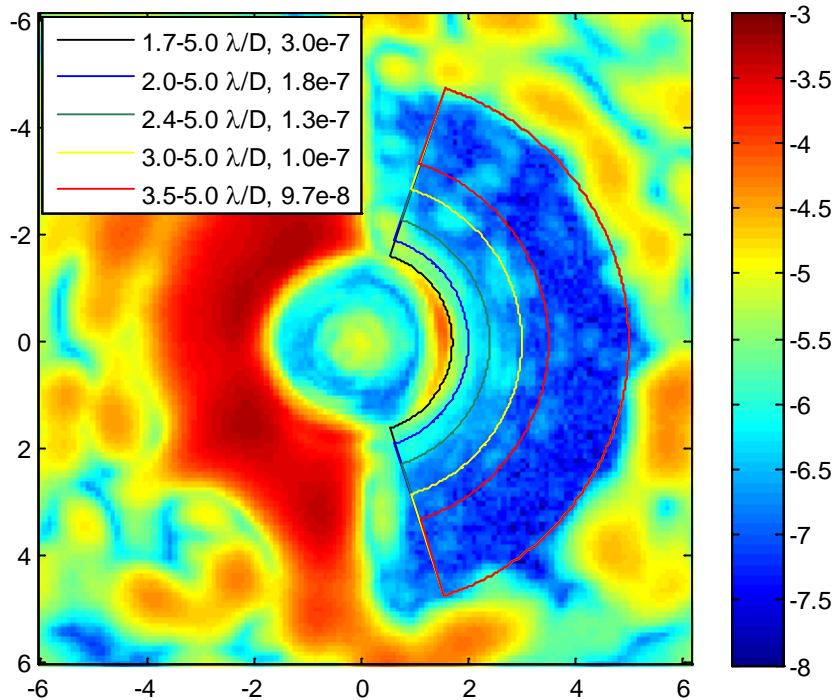
**Need deformable mirror with lots of actuators... in space.
The first time to try this is *not* on a \$1B space telescope.**



Single deformable mirror example



Log10 Contrast Ratio Planet/Star

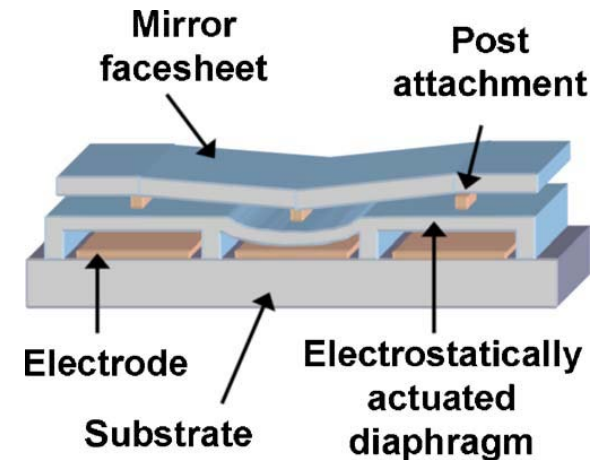
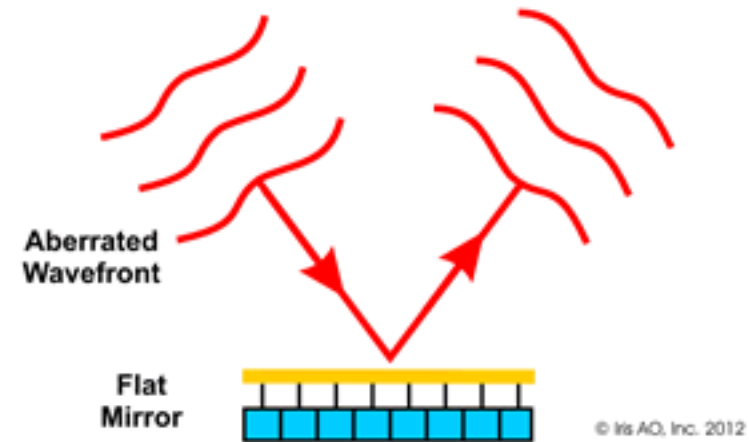
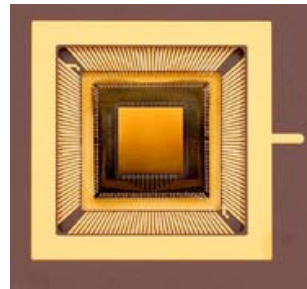


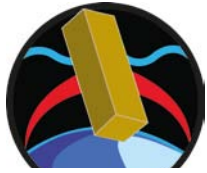
R. Belikov (NASA Ames), results with polarizer, 6/9/09 (in 2011, 5.4×10^{-8})

MEMS Deformable Mirrors

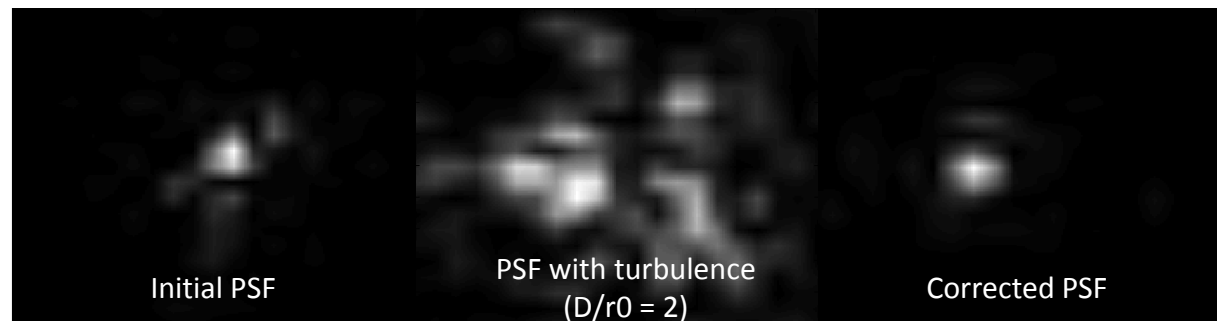
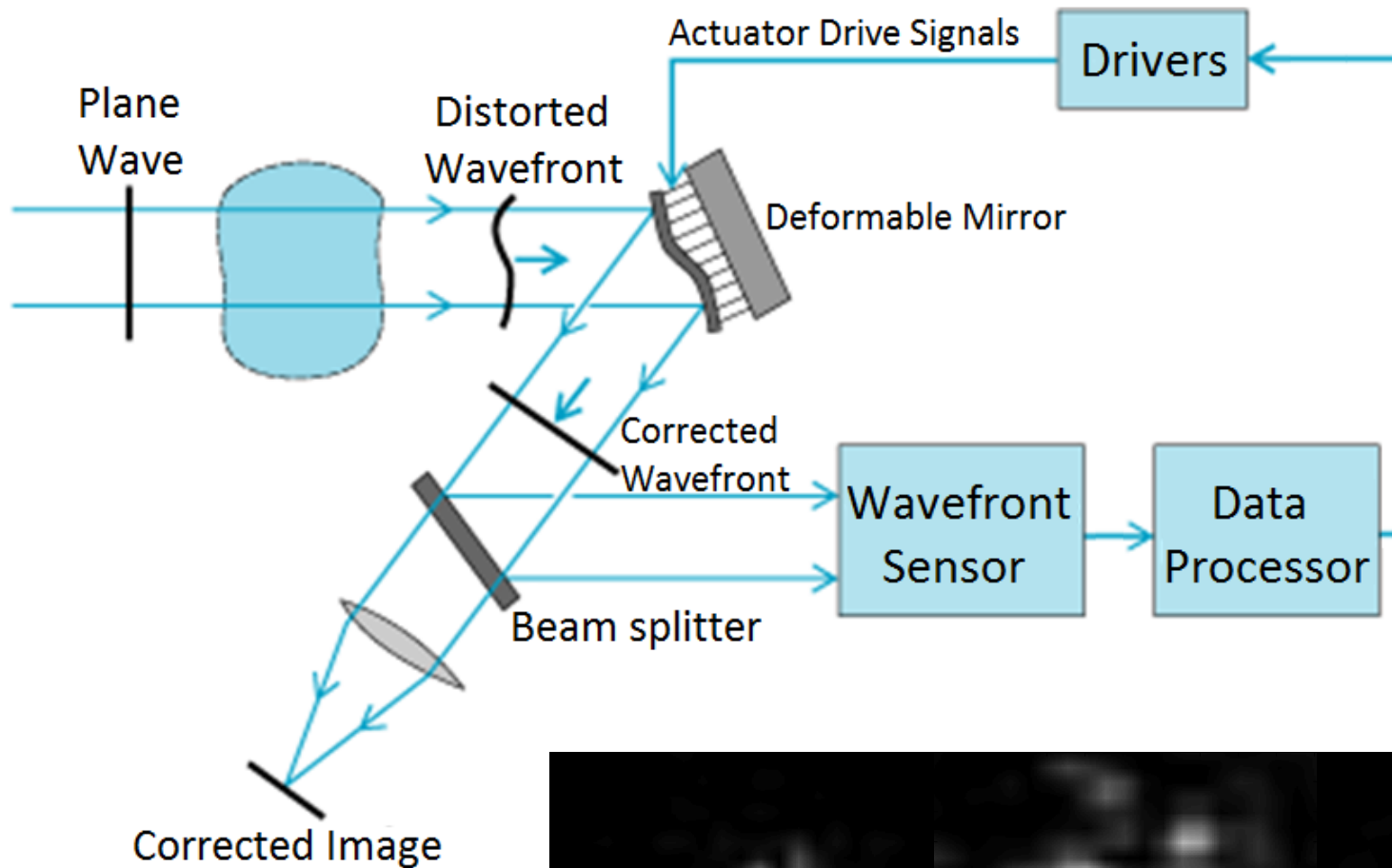


- Actuators change the shape of the mirror surface to match the incoming wavefront
- MEMS devices
 - Electrostatic actuators
 - Stroke of $\approx 1\text{--}8\ \mu\text{m}$
 - Higher voltage, low current
 - More actuators
 - Fast response time





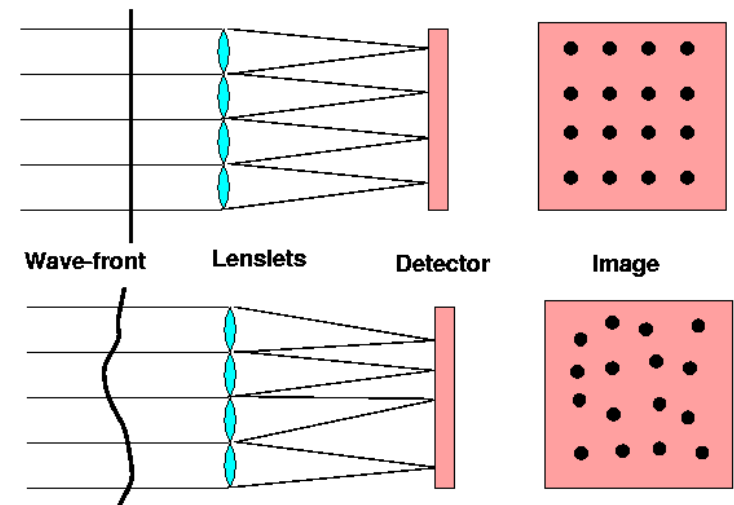
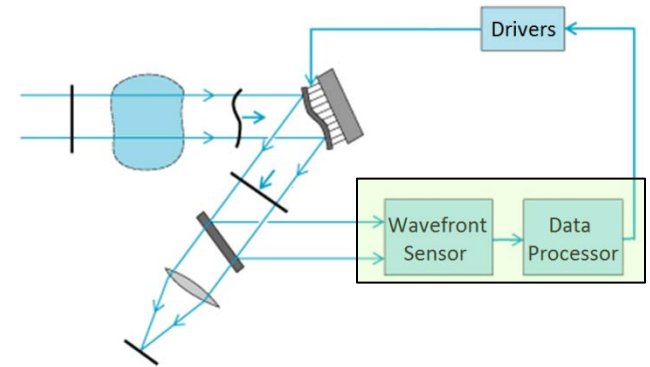
Wavefront Control System





Wavefront Control Sensors

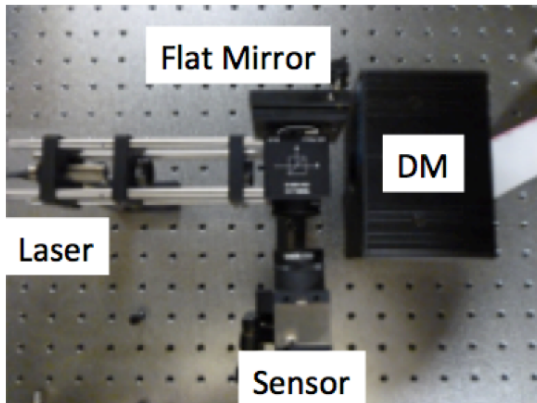
- Measure wavefront and calculate phase error to be corrected
- Sensored
 - Optical element introduced into beam to generate measurement
- Sensorless
 - Intensity-based measurements, computationally intensive



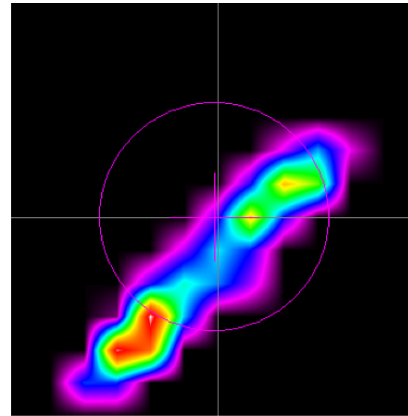


Lab prototype

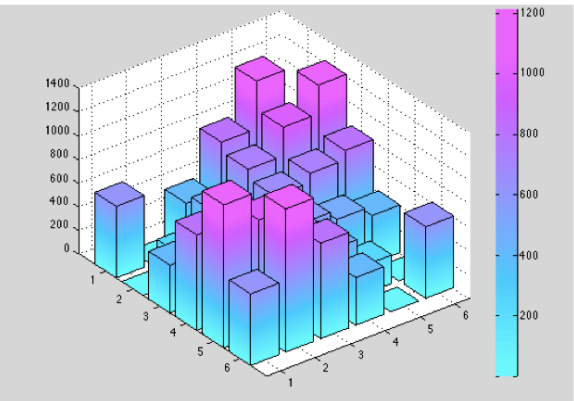
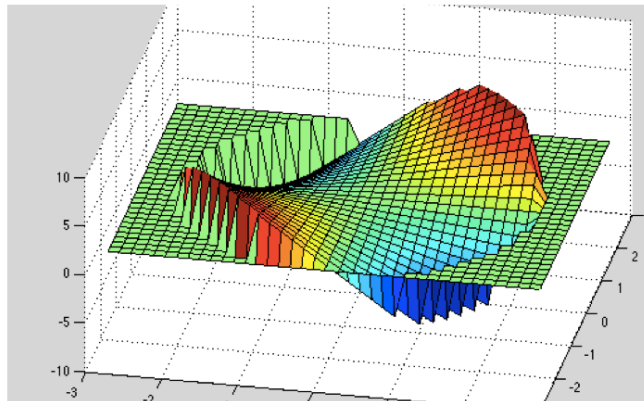
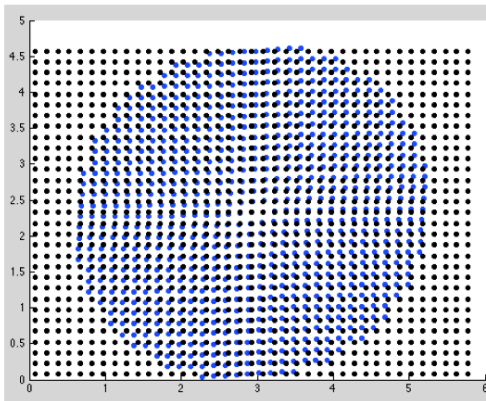
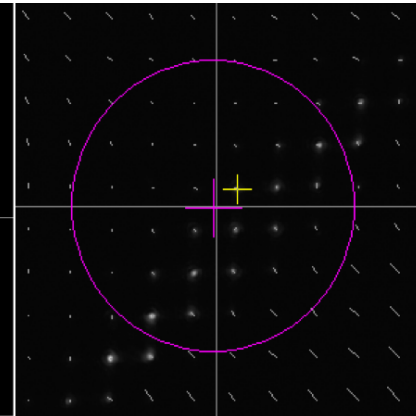
CubeSat-scale setup



$Z(2,-2), 2xy$



Shack Hartmann Spots

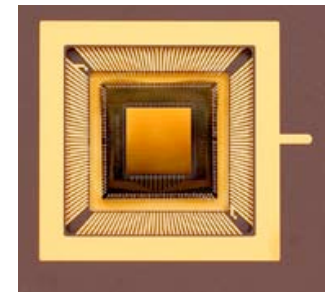
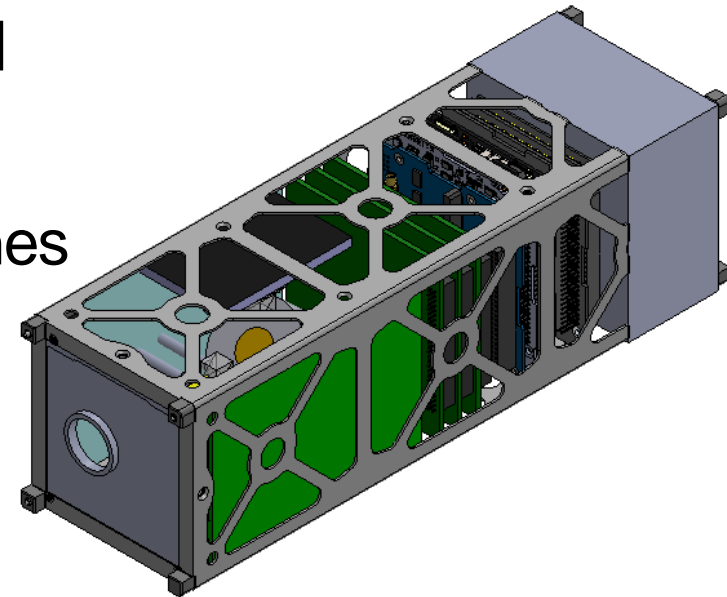


MATLAB simulation and controller



CubeSat Deformable Mirror Demonstration

- On-orbit performance of MEMS DM
- DMs will fit
 - Same actuator technology as big ones
 - BMC Mini MEMS DM, 32 actuators
 - Iris AO PTT111, 37 segment
 - Drive electronics board will also fit
- Laser Diode
 - “Easy” ADCS
 - Aperture can look at stars when laser off
 - But don’t really care which star(s)
 - Need only to have slew rate ~ 5 arcmin/s

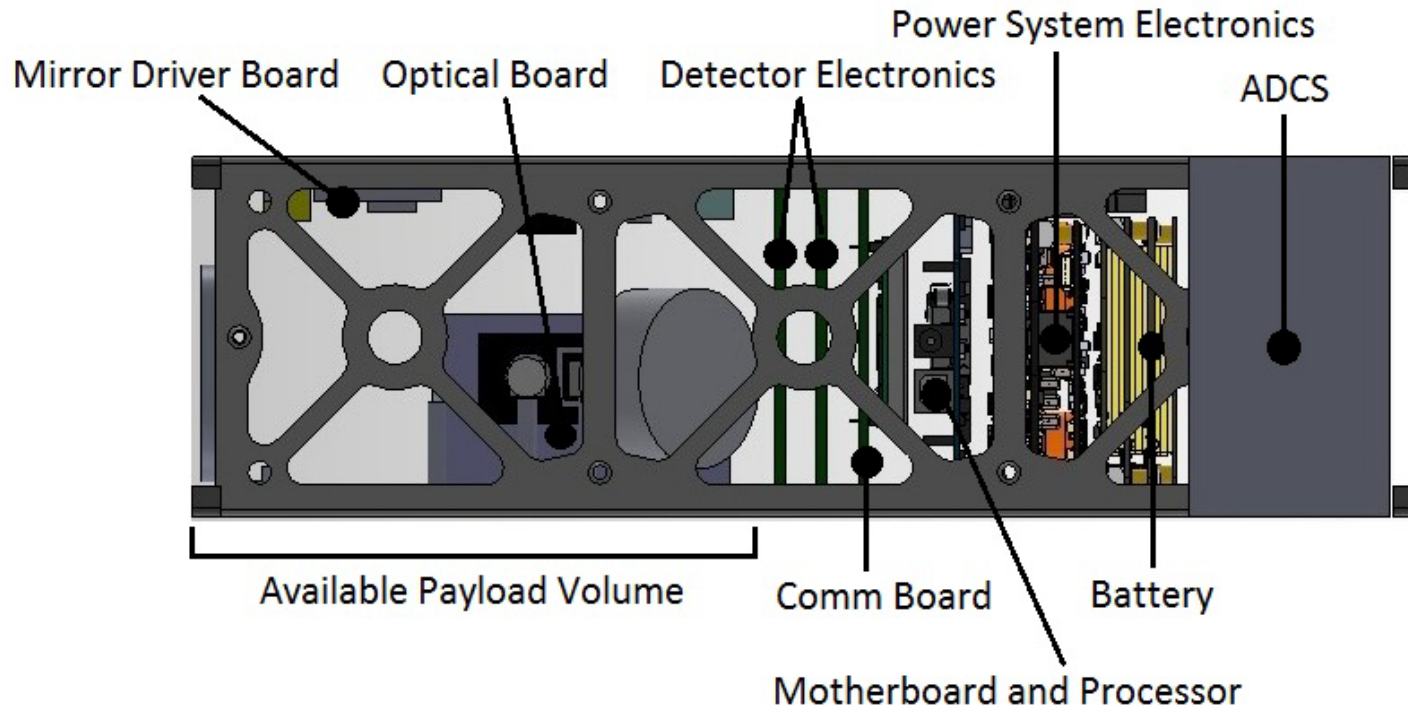


BMC MEMS DM



1.5 U Payload, 1.5 U Bus subsystems

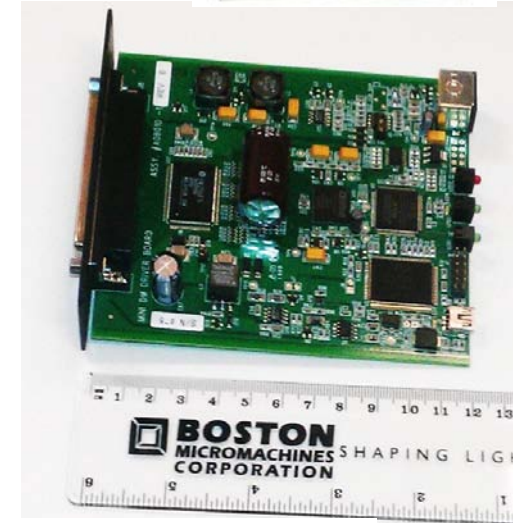
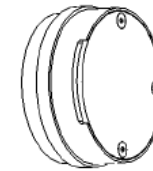
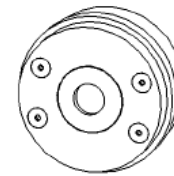
- Leveraging experience with MicroMAS, simpler ADCS





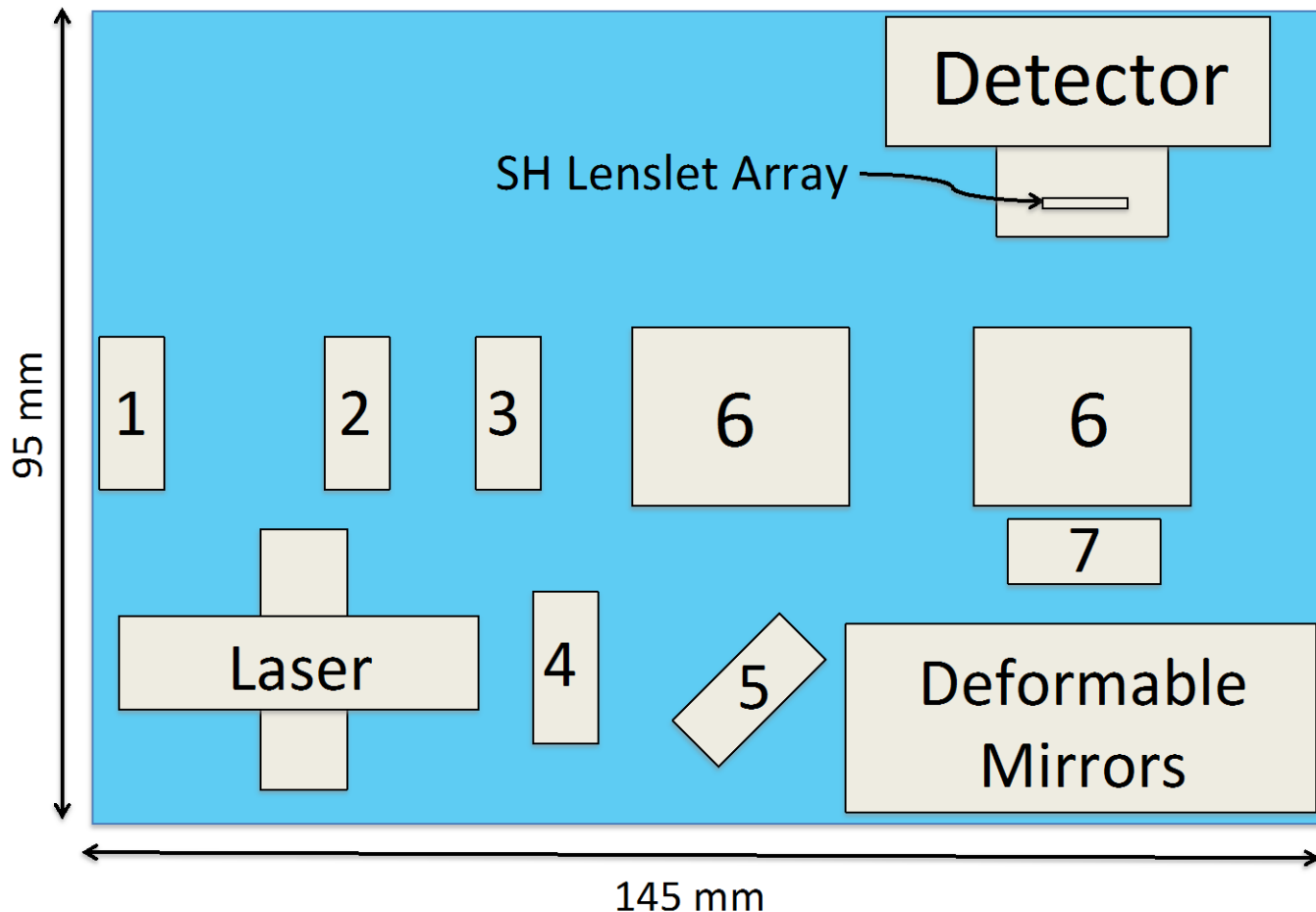
Payload Overview

- Boston Micromachines Mini MEMS DM
 - 32 actuators, 5 cm diameter, 2.21 cm tall
 - ~150 g including cables
 - Driver board
 - Existing board nearly CubeSat form factor
 - Straightforward to respin
- Optics
 - DM has ≥ 1.5 mm aperture
 - UV-grade fused silica
 - Lenses, beamsplitter, ND filters, lenslet array, quarter wave plate
 - Stress-free mounts, lens tubes
- Detector
 - IDS UI-5241LE-M, CMOS (or similar)
 - Closed loop wavefront control; processor





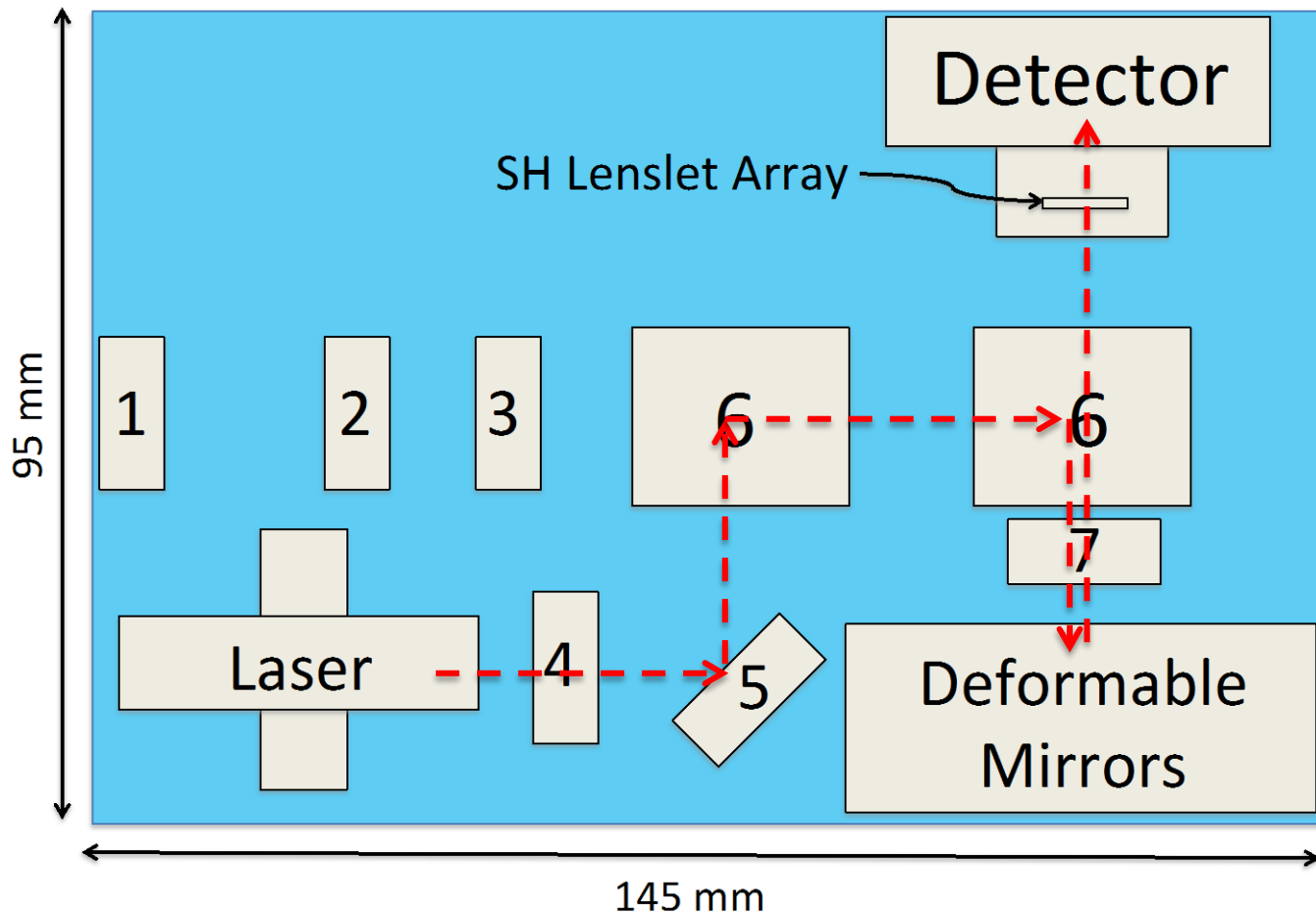
Shack-Hartmann Wavefront Sensing System



1. Aperture Lens
2. Collimating Lens
3. Polarizing Lens
4. Polarizing Lens
5. Flat Mirror
6. Beamsplitters
7. Quarter Waveplate



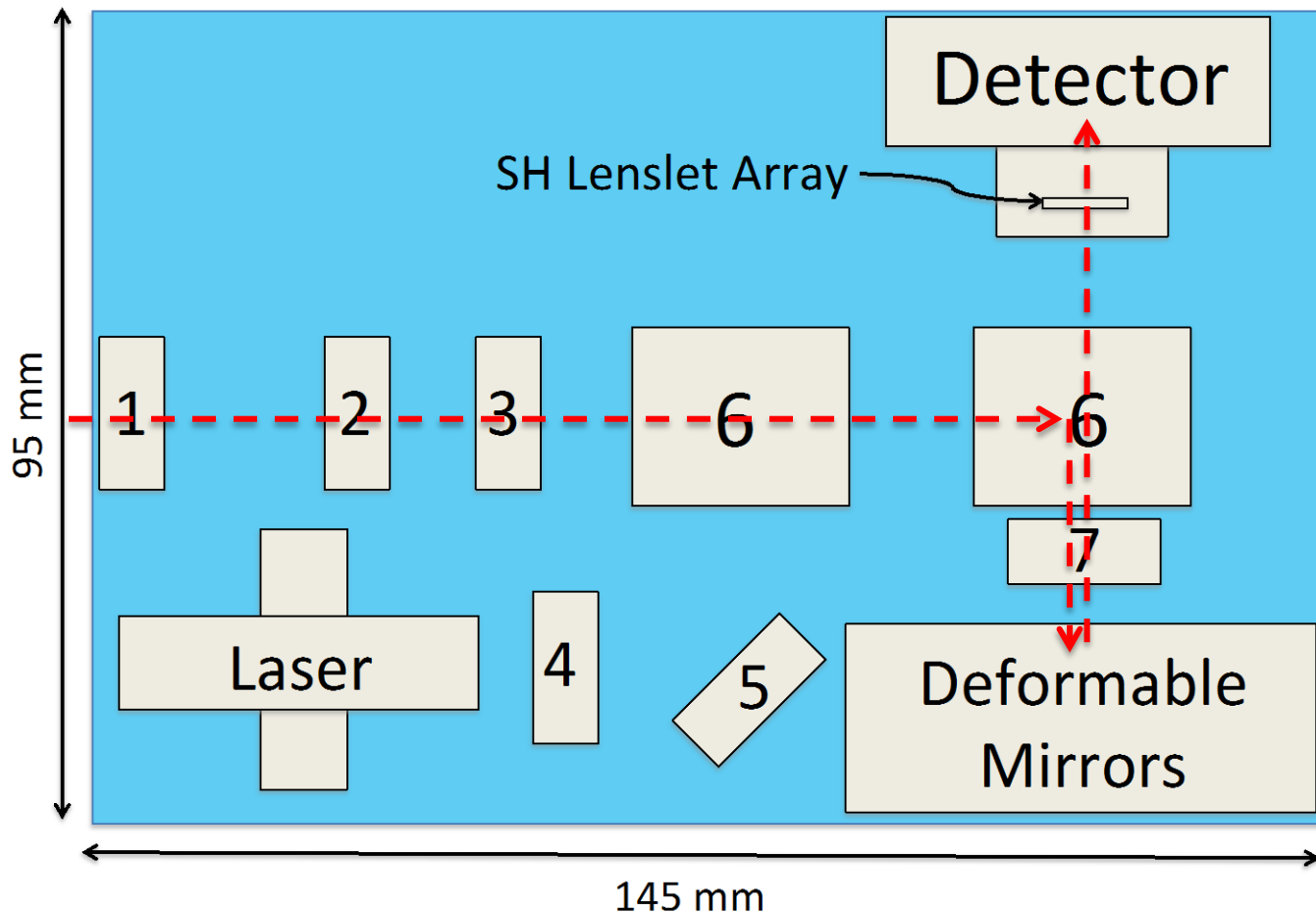
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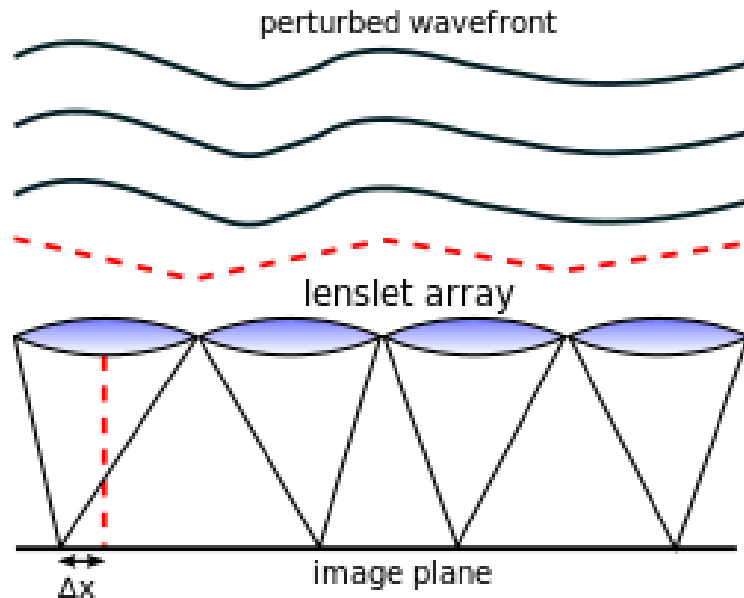
Shack-Hartmann Wavefront Sensing System



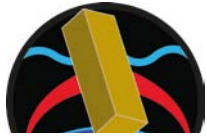
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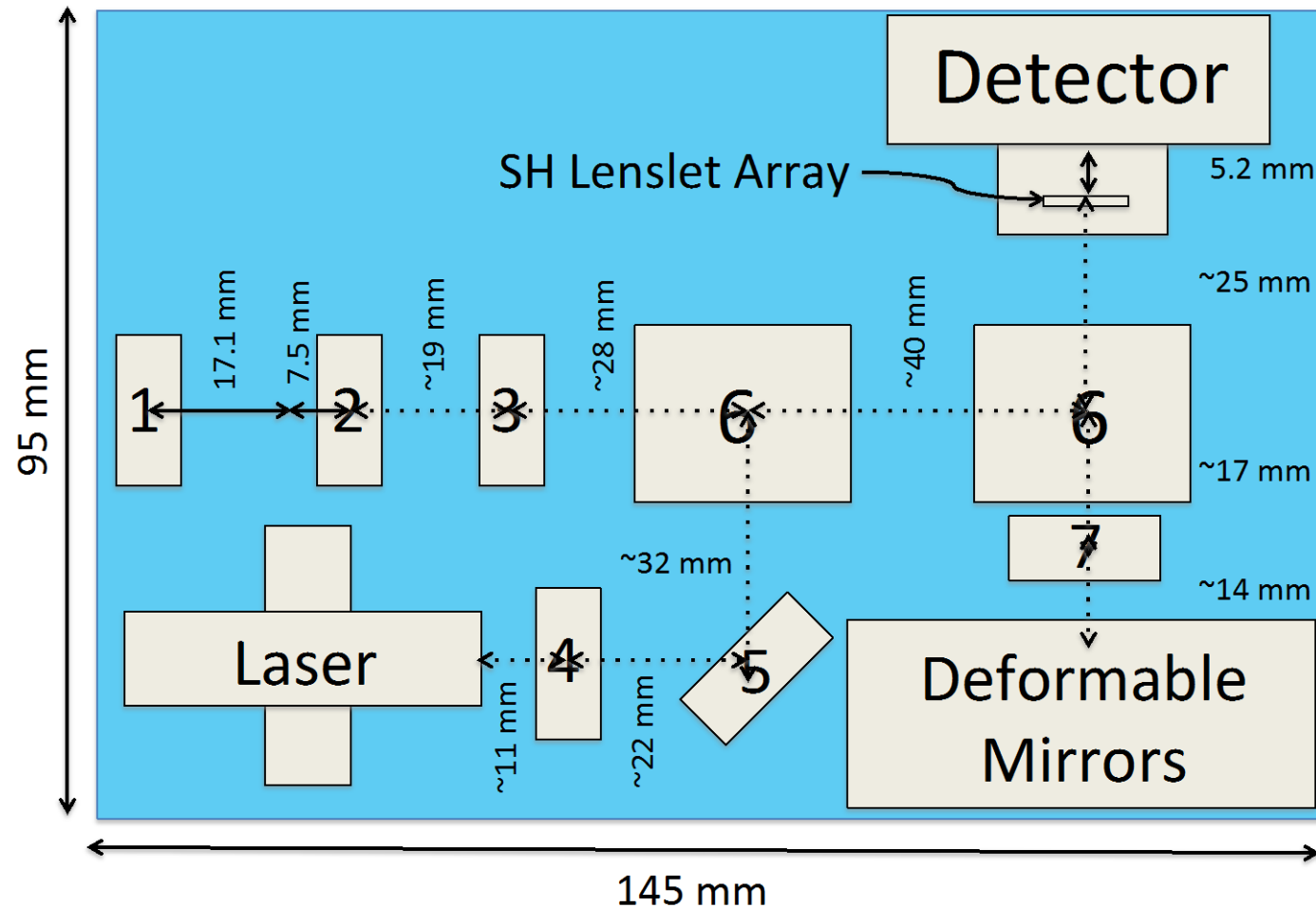
Shack-Hartmann Lenslet Array



- Incoming beam dictated by DM aperture
- Maximize sub-lenses / mm^2
- If lens is 10 mm x 10 mm, with 150 μm pitch = $\sim 67 \times 67$ spots.
So, for an incoming beam diameter of 2.25, about 15 x 15 spots.
- Need at least 4 pixels per spot, so for detector,
need the 2.25mm beam to cover more than 60 x 60 pixels.



Beam Divergence



$$\theta = 2 \arctan \left(\frac{D_f - D_i}{2L} \right)$$

Assumptions:

1. Beam is circular
2. No additional beam divergence through optical components



- Avionics Requirements
 - Camera interface / readout
 - Low frame rate image processing
 - Centroid, delta x and delta y, slope reconstruction
 - Linear algebra for mirror controller

- Possible solutions
 - PC104 form factor single board computer
 - Raspberry Pi
 - Also low-speed camera option
 - 5 MO OmniVision 5467 (60 fps at 720p)
 - ODroid-X2
 - ARM, standard peripherals



Raspberry Pi, Wikipedia



Hardkernel.com



- Laboratory development
 - Optical tolerancing, payload trades (Zemax)
 - Wavefront sensing, quantify DM reconstruction capability
 - Accuracy as function of # lenslets, alignment, tolerancing
 - Optimize wavefront reconstruction data products
 - Centroids, delta x, delta y, Zernike or Fourier coefficients
 - Update mirror drive electronics
 - Avionics design and testing
- Environmental tests on mirrors, drivers (ref. Shea et al. 2006)
 - Mechanical, electrical, follow up with ground efforts
- Partners, sponsors, launch opportunities, logistics



Design and build cost-effective, small wavefront control CubeSat to characterize high actuator-count **MEMS** deformable mirrors.

Enable implementation of active/adaptive optics with MEMS DMs on future space missions.

High contrast imaging.

Precision pointing.

Modulation.



Thank you!



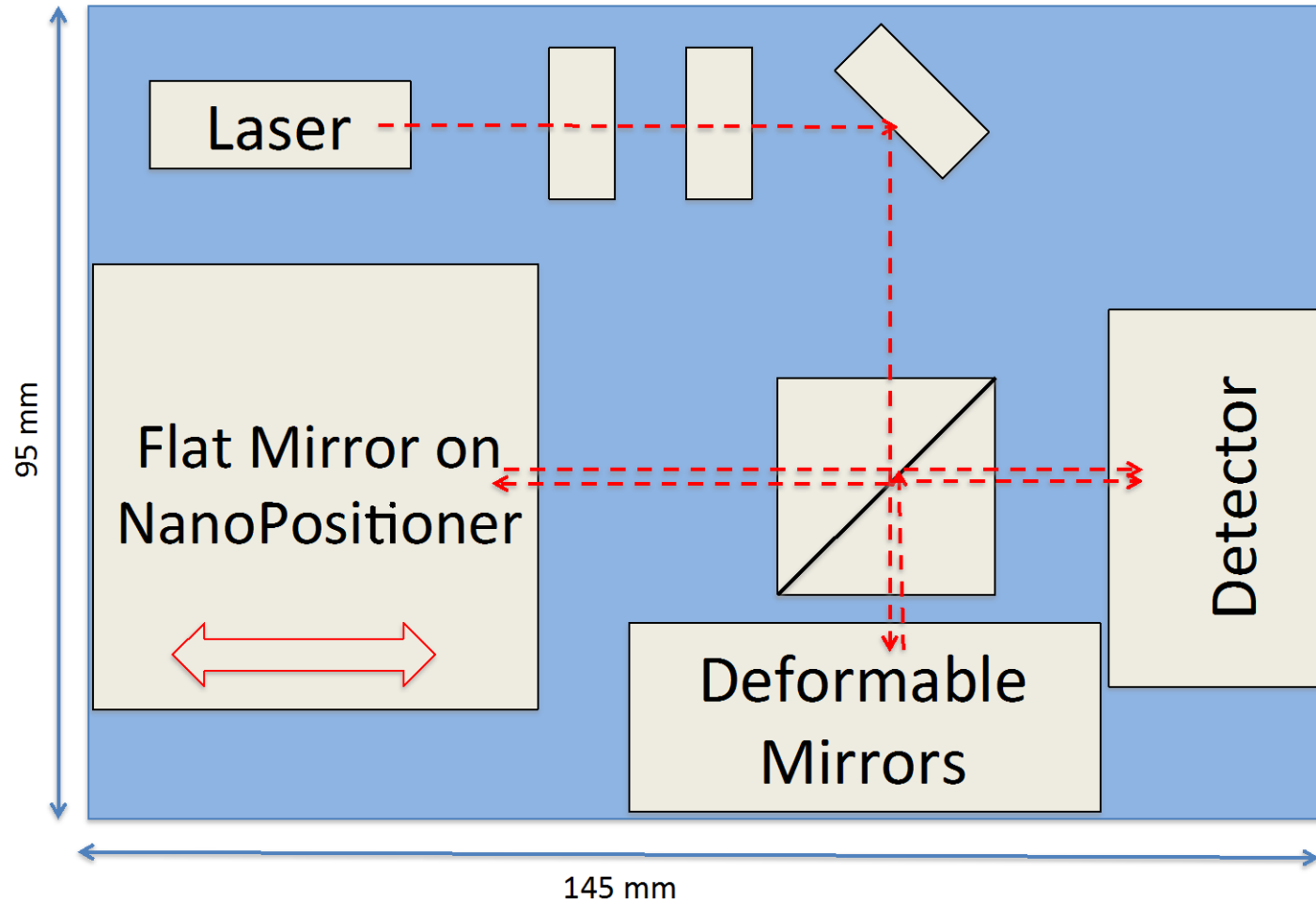
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<http://dx.doi.org/10.1364/BOE.3.000104>.
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- [14] University at Buffalo, 'GLADOS', University Nanosat Program 7 Flight Competition Review
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Backup Slides



Michelson Interferometer with Flat Mirror on NanoPositioner





Payload Requirements

ID	Statement	Relevant parts
PLD-1	The payload shall command a MEMS deformable mirror to run a pre-defined test sequence for at least 5 minutes [TBR] each orbit.	All
PLD-1.1	The payload shall have the ability to control any combination of actuators within 0.001 [TBR] seconds of each other, at a minimum rate of 100 Hz [TBR], with a minimum stroke of 1.5 microns, and with a precision of at least 1 nm [TBR].	Deformable Mirror
PLD-2	The payload shall have the ability to measure and reconstruct the optical wavefront at one wavelength for the duration of a 5 minute [TBR] test sequence each orbit.	Avionics Interface
PLD-2.1	The payload shall have the ability to measure the optical wavefront at a minimum rate of 100 Hz [TBR]	Detector, Avionics
PLD-2.2	The payload shall have the ability to reconstruct the optical wavefront with a minimum accuracy of 100 nm rms [TBR].	SH array, Detector



Example: Find beam diameter

Beam leaves laser with divergence Θ , and effective diameter D_i , and travels to polarizer, a distance L away. What is the beam diameter D_f entering the polarizer?

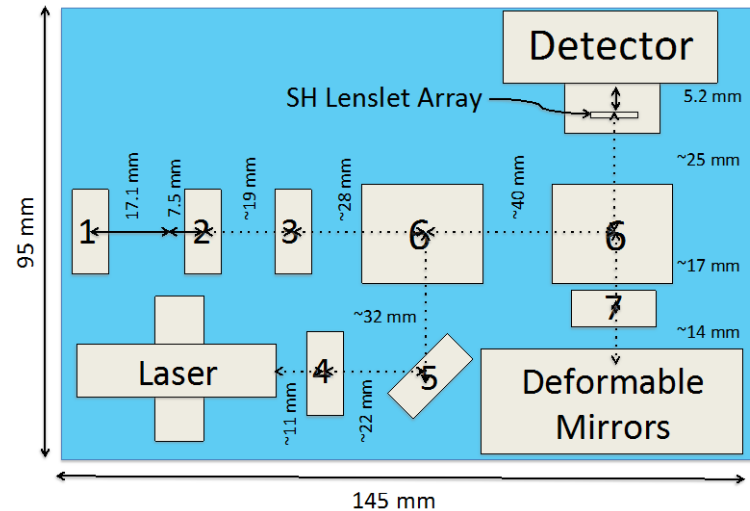
For the CPS186 laser:

- $\Theta \leq 1.8 \text{ mrad}$
- $D_i = 1.2309 \text{ mm}$

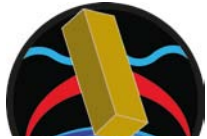
$$\Theta = 2 \arctan\left(\frac{D_f - D_i}{2L}\right)$$

$$(1.8 \text{ mrad}) = 2 \arctan\left(\frac{D_f - 1.2309 \text{ mm}}{2(11 \text{ mm})}\right)$$

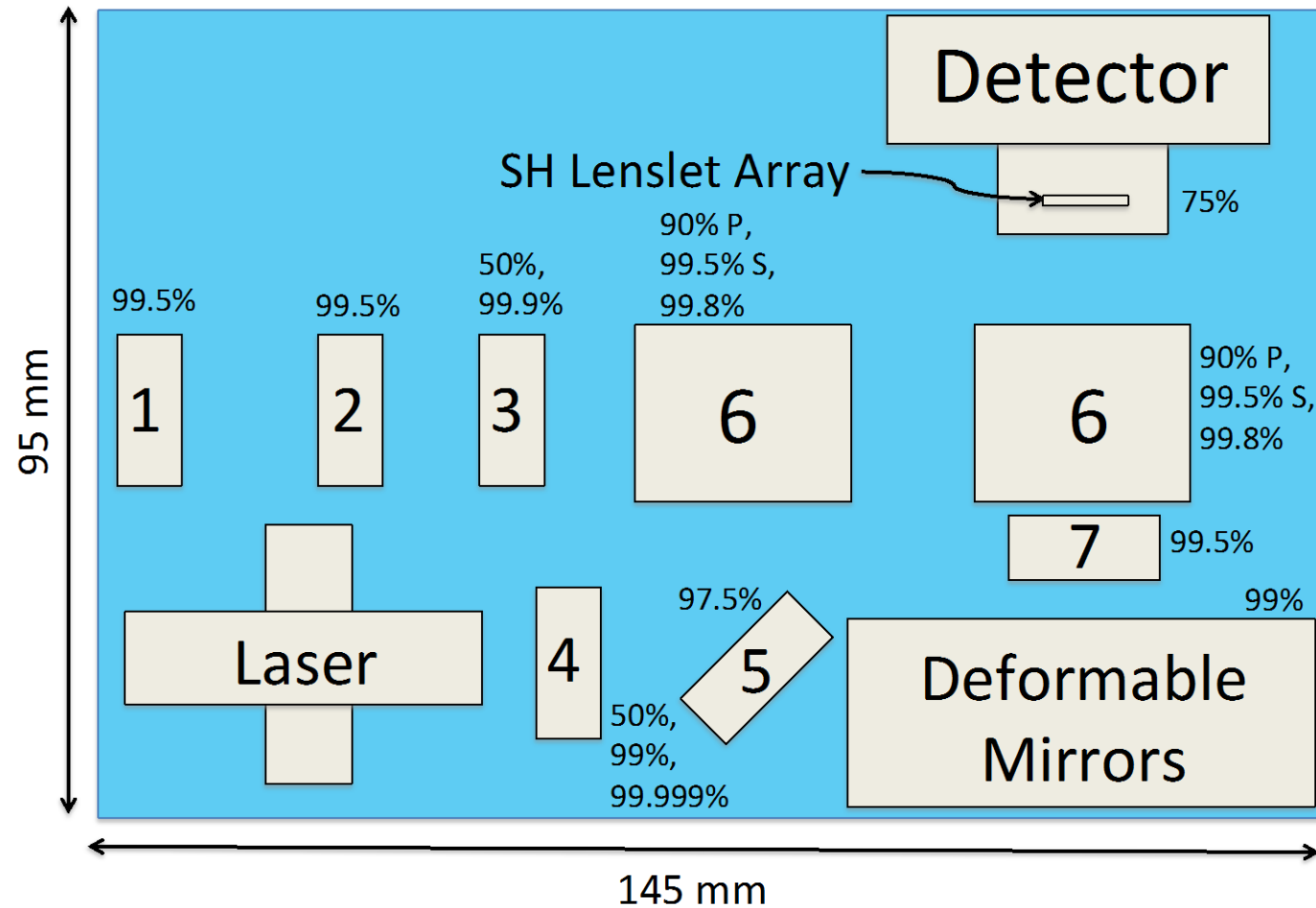
$$\therefore D_f = 2(11 \text{ mm}) \times \tan\left(\frac{1.8 \text{ mrad}}{2}\right) + 1.2309 \text{ mm} = 1.2507 \text{ mm}$$



At the detector:
 $D_f \approx 1.5859 \text{ mm}$



Absorption, Reflectivity, and Polarization



$$P = \int I \cdot dA$$

Assumptions:

1. Beam is circular
2. No power/intensity lost between components (small distances)



Example: Find beam intensity

Beam leaves laser with power P , and effective diameter D_i , and travels to polarizer. What is the beam intensity after going through the polarizer?

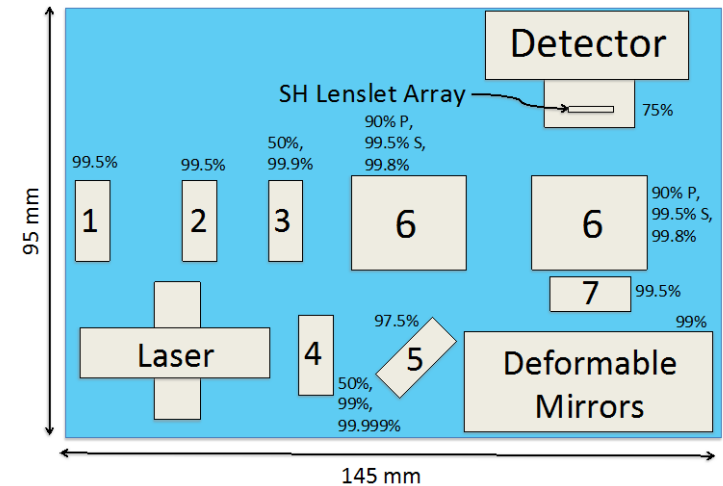
For the CPS186 laser:

- $P = 4.70 \text{ mW}$
- $D_i = 1.2309 \text{ mm}$

$$P_i = \int I_i \cdot dA$$

$$P_i \approx I_i (\pi r_i^2)$$

$$\therefore I_i \approx \frac{P_i}{\pi \left(\frac{D_i}{2}\right)^2} = \frac{4.7 \text{ mW}}{\pi \left(\frac{1.2309 \text{ mm}}{2}\right)^2} = 3.9497 \text{ mW} / \text{mm}^2$$



At the detector:

$$I_f \approx 1.2411 \text{ mW/mm}^2$$

$$P \approx 2.4514 \text{ mW}$$



Analysis & Design

Actuator:

3- orthogonal torque coils

- Light weight, low power actuator
- Provide actuation for active magnetic control

Sensors

• Magnetometer

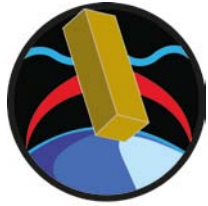
- Provide reading of local magnetic field for magnetic control
- Provide attitude knowledge in eclipse

• Sun Sensors

- Provide attitude knowledge in daytime

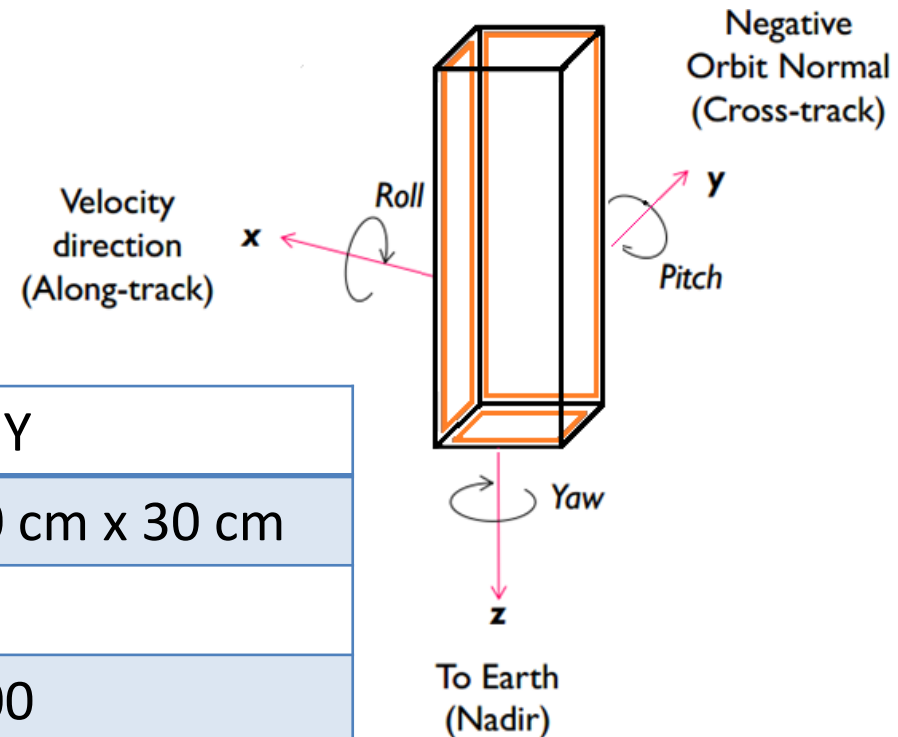
• IMU

- Provide angular rate knowledge for vibration damping



Torque Coil Design

Total Mass	520 g
Max Total Power	1.35 W



Direction	Z	X, Y
Size	10 cm × 10 cm	10 cm x 30 cm
Quantity	1	2
Turns	500	400
Current	0.12 A	0.04 A
Wire Gauge	28 AWG	28 AWG
Magnetic moment	0.60 A*m ²	0.60 A*m ²